

Corrigenda for 2024 Classification Technical Rules



* Please note that this corrigenda is for the printed version of the 2024 Classification Technical Rules, and the PDF files posted on the website have been corrected.

PART 1

Present	Amendments	Reason
<p style="text-align: center;"><Guidance Part 1></p> <p style="text-align: center;">Annex 1-12 Hull Survey for Classification Survey during Construction</p> <p>Table 1 Hull Surveyable Items Activities Table</p> <p>< Supplement of Table 1 ></p> <p>– Prior to commencement of survey for any newbuilding project, the Society is to discuss with the shipbuilder at a kick off meeting the items listed in Table 1. The purpose of the meeting is to review and agree how the list of specific activities shown in Table 1 is to be addressed. The meeting is to take into account the shipbuilder's construction facilities and ship type including the list of proposed subcontractors.</p> <p style="padding-left: 40px;"><omitted></p> <p>– In the event of series ship production*, the requirement for a kick off meeting may be waived for the second and subsequent ships provided that no changes to the specific activities agreed in the kick off meeting for the first ship are introduced. If any changes are introduced, these are to be agreed in a new dedicated meeting and documented in a record of such meeting.</p> <p>* Series Ship: See Pt 1, Ch 1, 309. of the Rules.</p>	<p style="text-align: center;"><Guidance Part 1></p> <p style="text-align: center;">Annex 1-12 Hull Survey for Classification Survey during Construction</p> <p>Table 1 Hull Surveyable Items Activities Table</p> <p>< Supplement of Table 1 ></p> <p>– Prior to commencement of survey for any newbuilding project, the Society is to discuss with the shipbuilder at a kick off meeting the items listed in Table 1. The purpose of the meeting is to review and agree how the list of specific activities shown in Table 1 is to be addressed. The meeting is to take into account the shipbuilder's construction facilities and ship type including the list of proposed subcontractors.</p> <p style="padding-left: 40px;"><same as the current Guidance></p> <p>– In the event of series ship production*, the requirement for a kick off meeting may be waived for the second and subsequent ships provided that no changes to the specific activities agreed in the kick off meeting for the first ship are introduced. If any changes are introduced, these are to be agreed in a new dedicated meeting and documented in a record of such meeting.</p> <p>* Series Ship: See Pt 1, Ch 1, 101. 5. 309. of the Rules.</p>	<p>–At the request of the Survey Team's letter(SUR3000-582-2024) on April 24 2024.</p>

Present	Amendment	Note
<p style="text-align: center;">Present 〈Rules〉 Pt 1</p> <p style="text-align: center;">CHAPTER 3 HULL SURVEYS OF SHIPS ~</p> <p style="text-align: center;">Section 2 Bulk Carries</p> <p>202. Annual Survey</p> <p>3. Examination of weather decks, hatch covers and coamings</p> <p>(4) Where the cargo hatch securing system does not function properly, repairs are to be carried out under the supervision of the Society. Where hatch covers or coamings undergo substantial repairs, the strength of securing devices should be upgraded to comply with Rules Pt 7, Ch 3, Sec 9, 905. "Securing arrangements". (2019)</p> <p style="text-align: center;">Section 6 Double Skin Bulk Carriers</p> <p>602. Annual Survey</p> <p>3. Examination of weather deck, hatch covers and coamings</p> <p>(4) Where the cargo hatch securing system does not function properly, repairs are to be carried out under the supervision of the Society. Where hatch covers or coamings undergo substantial repairs, the strength of securing devices should be upgraded to comply with Rules Pt 7, Ch 3, Sec 9, 905. "Securing arrangements". (2019)</p>	<p style="text-align: center;">Amendment 〈Rules〉 Pt 1</p> <p style="text-align: center;">CHAPTER 3 HULL SURVEYS OF SHIPS ~</p> <p style="text-align: center;">Section 2 Bulk Carries</p> <p>202. Annual Survey</p> <p>3. Examination of weather decks, hatch covers and coamings</p> <p>(4) Where the cargo hatch securing system does not function properly, repairs are to be carried out under the supervision of the Society. Where hatch covers or coamings undergo substantial repairs, the strength of securing devices should be upgraded to comply with Rules Pt 4, Ch 2, Sec 5. (2019)</p> <p style="text-align: center;">Section 6 Double Skin Bulk Carriers</p> <p>602. Annual Survey</p> <p>3. Examination of weather deck, hatch covers and coamings</p> <p>(4) Where the cargo hatch securing system does not function properly, repairs are to be carried out under the supervision of the Society. Where hatch covers or coamings undergo substantial repairs, the strength of securing devices should be upgraded to comply with Rules Pt 4, Ch 2, Sec 5. (2019)</p>	

Present	Amendment	Note
<p style="text-align: center;">Present 〈Guidance〉 Pt 1</p> <p>Annex 1-5 Thickness Measurement Method for Hull Structural Members</p> <p>2. Wear Limit</p> <p>(3) Wear limit of hold hatch cover of bulk carriers which are contracted for construction after 1st July 1998 and before 1st January 2004 and designed by the Rules Pt 7, Ch 3, Sec 9 is to be determined in accordance with the following requirements.</p> <p>(4) Wear limit of hold hatch cover and hatch coatings of all bulk carriers, ore carriers and combination carriers which are contracted for construction on or after 1st January 2004 and designed by the Rules Pt 7, Ch 3, Sec 9 is to be determined in accordance with the following requirements.</p>	<p style="text-align: center;">Amendment 〈Guidance〉 Pt 1</p> <p>Annex 1-5 Thickness Measurement Method for Hull Structural Members</p> <p>2. Wear Limit</p> <p>(3) Wear limit of hold hatch cover of bulk carriers which are contracted for construction after 1st July 1998 and before 1st January 2004 and designed by the Rules Pt 4, Ch 2 is to be determined in accordance with the following requirements.</p> <p>(4) Wear limit of hold hatch cover and hatch coatings of all bulk carriers, ore carriers and combination carriers which are contracted for construction on or after 1st January 2004 and designed by the Rules Pt 4, Ch 2 is to be determined in accordance with the following requirements.</p>	

PART 2

Present	Amendment	Note
<p style="text-align: center;"><Rules> Pt 2</p> <p style="text-align: center;">CHAPTER 1 MATERIALS</p> <p style="text-align: center;">Section 4 Welding Procedure Qualification Tests</p> <p>304. Rolled steels for low temperature service</p> <p>10. Marking</p> <p>(1) Steels which have satisfactorily complied with the required tests are to be marked with the identification mark in accordance with the requirements in 110.</p> <p>(2) For steels to which the requirements given in Notes (1) of Table 2.1.17 and Notes (7) of Table 2.1.17-1 have been applied, "TM" and impact test temperature "T" are to be suffixed to the markings. (e.g. <i>RL 325TM-50T</i>)</p> <p>(3) For steel to which the requirements given in 5. (3), the specified value of the maximum yield stress or proof stress and "A" are to be suffixed to the markings. (e.g. <i>RL 325A-440A (2023)</i>)</p>	<p style="text-align: center;"><Rules> Pt 2</p> <p style="text-align: center;">CHAPTER 1 MATERIALS</p> <p style="text-align: center;">Section 4 Welding Procedure Qualification Tests</p> <p>304. Rolled steels for low temperature service</p> <p>10. Marking</p> <p>(1) Steels which have satisfactorily complied with the required tests are to be marked with the identification mark in accordance with the requirements in 110.</p> <p>(2) For steels to which the requirements given in Notes (2) of Table 2.1.17 and Notes (7) of Table 2.1.18 have been applied, "TM" and impact test temperature "T" are to be suffixed to the markings. (e.g. <i>RL 325TM-50T</i>)</p> <p>(3) For steel to which the requirements given in 5. (3), the specified value of the maximum yield stress or proof stress and "A" are to be suffixed to the markings. (e.g. <i>RL 325A-440A (2023)</i>)</p>	<p>Date: 2024.07.19. Person in charge: Choi Daegon</p> <p>Typo</p>

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<p style="text-align: center;"><Rules> Pt 2</p> <p style="text-align: center;">CHAPTER 2 WELDING</p> <p style="text-align: center;">Section 4 Welding Procedure Qualification Tests</p> <p>404. Tests for butt welded joints</p> <p>4. Tensile tests</p> <p>Table 2.2.6 Tensile Test Requirements for Butt Welded Joint</p> <table border="1" data-bbox="125 671 943 1278"> <thead> <tr> <th>Kind of testing materials</th> <th>Grade of testing materials</th> <th>Tensile strength (N/mm²)</th> <th>Yield strength (N/mm²)</th> </tr> </thead> <tbody> <tr> <td rowspan="2">Rolled steels for lower temperature service</td> <td rowspan="2">RL 9M490</td> <td>590 min.⁽¹⁾</td> <td>315 min.</td> </tr> <tr> <td>630 min.⁽²⁾</td> <td>-</td> </tr> <tr> <td>Steel pipes for low temperature service</td> <td>RLP9</td> <td>630 min.</td> <td>-</td> </tr> <tr> <td rowspan="6">Aluminium alloys</td> <td>5754</td> <td>190 min.</td> <td>-</td> </tr> <tr> <td>5086</td> <td>240 min.</td> <td>-</td> </tr> <tr> <td>5083</td> <td>275 min.</td> <td>-</td> </tr> <tr> <td>5383</td> <td>290 min.</td> <td>-</td> </tr> <tr> <td>5059</td> <td>330 min.</td> <td>-</td> </tr> <tr> <td>6005A, 6061, 6082⁽³⁾</td> <td>170 min.</td> <td>-</td> </tr> </tbody> </table> <p>(Notes) (1) For test specimen in longitudinal direction (2) For test specimen in transverse direction (3) See notes (9) of Table 2.2.4.</p>	Kind of testing materials	Grade of testing materials	Tensile strength (N/mm ²)	Yield strength (N/mm ²)	Rolled steels for lower temperature service	RL 9M490	590 min. ⁽¹⁾	315 min.	630 min. ⁽²⁾	-	Steel pipes for low temperature service	RLP9	630 min.	-	Aluminium alloys	5754	190 min.	-	5086	240 min.	-	5083	275 min.	-	5383	290 min.	-	5059	330 min.	-	6005A, 6061, 6082 ⁽³⁾	170 min.	-	<p style="text-align: center;"><Rules> Pt 2</p> <p style="text-align: center;">CHAPTER 2 WELDING</p> <p style="text-align: center;">Section 4 Welding Procedure Qualification Tests</p> <p>404. Tests for butt welded joints</p> <p>4. Tensile tests</p> <p>Table 2.2.6 Tensile Test Requirements for Butt Welded Joint</p> <table border="1" data-bbox="994 671 1809 1278"> <thead> <tr> <th>Kind of testing materials</th> <th>Grade of testing materials</th> <th>Tensile strength (N/mm²)</th> <th>Yield strength (N/mm²)</th> </tr> </thead> <tbody> <tr> <td rowspan="2">Rolled steels for lower temperature service</td> <td rowspan="2">RL 9M490</td> <td>590 min.⁽¹⁾</td> <td>315 min.</td> </tr> <tr> <td>630 min.⁽²⁾</td> <td>-</td> </tr> <tr> <td>Steel pipes for low temperature service</td> <td>RLP9</td> <td>630 min.</td> <td>-</td> </tr> <tr> <td rowspan="6">Aluminium alloys</td> <td>5754</td> <td>190 min.</td> <td>-</td> </tr> <tr> <td>5086</td> <td>240 min.</td> <td>-</td> </tr> <tr> <td>5083</td> <td>275 min.</td> <td>-</td> </tr> <tr> <td>5383</td> <td>290 min.</td> <td>-</td> </tr> <tr> <td>5059</td> <td>330 min.</td> <td>-</td> </tr> <tr> <td>6005A, 6061, 6082⁽³⁾</td> <td>170 min.</td> <td>-</td> </tr> </tbody> </table> <p>(Notes) (1) For test specimen in longitudinal direction (2) For test specimen in transverse direction (3) See notes (8) of Table 2.2.4.</p>	Kind of testing materials	Grade of testing materials	Tensile strength (N/mm ²)	Yield strength (N/mm ²)	Rolled steels for lower temperature service	RL 9M490	590 min. ⁽¹⁾	315 min.	630 min. ⁽²⁾	-	Steel pipes for low temperature service	RLP9	630 min.	-	Aluminium alloys	5754	190 min.	-	5086	240 min.	-	5083	275 min.	-	5383	290 min.	-	5059	330 min.	-	6005A, 6061, 6082 ⁽³⁾	170 min.	-	<p>Date: 2024.07.19. Person in charge: Choi Daegon</p> <p style="text-align: right;">Typo</p>
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Present	Amendment	Note
<p style="text-align: center;"> 〈Guidance〉 Pt 2 CHAPTER 2 WELDING Section 1 General </p> <p>103. Special weldings</p> <p>5. Test specimens</p> <p>(3) Impact test specimens are to be the charpy V-notch test specimen specified in Table 2.1.3 of the Rules. In the impact test, one set of test specimens comprising three pieces are to be taken from every test assembly. The test specimens are to be taken alternately from the position "a" and from a position among "b" through "e" where the lowest value is recorded in the welding procedure qualification test, shows in Fig 2.2.7 of the Rules. This means that one set of three test specimens are taken from a test assembly at the position "a", hence other set of three test specimens are taken in the subsequent test assembly from the position among "b" through "e" where the lowest value is recorded, and this procedure is repeated. No impact test specimens is required in cases of stainless steel and aluminium alloy.</p>	<p style="text-align: center;"> 〈Guidance〉 Pt 2 CHAPTER 2 WELDING Section 1 General </p> <p>103. Special weldings</p> <p>5. Test specimens</p> <p>(3) Impact test specimens are to be the charpy V-notch test specimen specified in Table 2.1.3 of the Rules. In the impact test, one set of test specimens comprising three pieces are to be taken from every test assembly. The test specimens are to be taken alternately from the position "a" and from a position among "b" through "e" where the lowest value is recorded in the welding procedure qualification test, shows in Fig 2.2.8 of the Rules. This means that one set of three test specimens are taken from a test assembly at the position "a", hence other set of three test specimens are taken in the subsequent test assembly from the position among "b" through "e" where the lowest value is recorded, and this procedure is repeated. No impact test specimens is required in cases of stainless steel and aluminium alloy.</p>	<p>Date: 2024.07.19. Person in charge: Choi Daegon</p> <p>Typo</p>

PART 3

Present	Amendment	Reason
<p style="text-align: center;">〈Guidance Pt.3〉</p> <p style="text-align: center;">Annex 3–3 Guidance for the Fatigue Strength Assessment of Ship Structures</p> <p>1. General <i>(2020)</i> 〈omitted〉</p> <p>2. Definition of stress</p> <p>In the fatigue analysis, three kinds of stresses; i. e. the nominal stress, the hot spot stress and notch stress can be used. The hot spot stress approach and edge stress approach are to be employed in this Guidance.</p> <p>(1) Nominal stress 〈omitted〉</p> <p>(2) Hot spot stress</p> <p>(A) 〈omitted〉</p> <p>(B) For the calculation of the hot spot stress, multiplying notch stress by stress concentration factor or the three dimensional finite element analysis is to be performed. Then, it can be determined by extrapolating maximum principal stresses outside the region affected by the weld geometry. The stress range near welding toe is to be used consistently depending on the effect by type and size of the finite element.</p> <p>(3) ~ (4) 〈omitted〉</p> <p>4. ~ 7. 〈omitted〉 ↓</p>	<p style="text-align: center;">〈Guidance Pt.3〉</p> <p style="text-align: center;">Annex 3–3 Guidance for the Fatigue Strength Assessment of Ship Structures</p> <p>1. General <i>(2020)</i> 〈same as the current Rules〉</p> <p>2. Definition of stress</p> <p>In the fatigue analysis, three kinds of stresses; i. e. the nominal stress, the hot spot stress and notch stress can be used. The hot spot stress approach and edge stress approach are to be employed in this Guidance.</p> <p>(1) Nominal stress 〈same as the current Rules〉</p> <p>(2) Hot spot stress</p> <p>(A) 〈same as the current Rules〉</p> <p>(B) For the calculation of the hot spot stress, multiplying nominal stress by stress concentration factor or the three dimensional finite element analysis is to be performed. Then, it can be determined by extrapolating maximum principal stresses outside the region affected by the weld geometry. The stress range near welding toe is to be used consistently depending on the effect by type and size of the finite element.</p> <p>(3) ~ (4) 〈same as the current Rules〉</p> <p>4. ~ 7. 〈same as the current Rules〉 ↓</p>	<p style="text-align: center;">- Typo</p>

PART 4

Present	Amendment	Note
<p style="text-align: center;">〈Guidance Part 4〉</p> <p style="text-align: center;">CHAPTER 1 RUDDERS</p> <p style="text-align: center;">Section 4 Rudder Strength Calculation</p> <p>401. Rudder strength calculation [See Rule]</p> <p>1. ~ 6. 〈omitted〉</p> <p>7. Type E rudders(Semi spade rudder with 2-conjugate elastic support)</p> <p>(1) General data The data on the semi spade rudder with 2-conjugate elastic support models is as follows(See Fig 4.1.7 and Fig 4.1.8 of the Guidance): K_{11}, K_{22}, K_{12} : Rudder horn compliance constants calculated for rudder horn with 2-conjugate elastic supports The 2-conjugate elastic supports are defined in terms of horizontal displacements, y_i, by the following equations:</p> <p style="padding-left: 40px;">at the lower rudder horn bearing: $y_1 = K_{12}B_2 - K_{22}B_1$ at the upper rudder horn bearing: $y_2 = K_{11}B_2 - K_{12}B_1$</p> <p>$y_1, y_2$: Horizontal displacements at the lower and upper rudder horn bearings, respectively (m) B_1, B_2 : Horizontal support forces at the lower and upper rudder horn bearings, respectively (kN) K_{11}, K_{22}, K_{12} : Obtained, in m/kN, from the following formulae:</p> $K_{11} = 1.3 \frac{\lambda^3}{3EJ_{1h}} + \frac{e^2\lambda}{GJ_{th}}$ $K_{22} = 1.3 \left[\frac{\lambda^3}{3EJ_{1h}} + \frac{\lambda^2(d-\lambda)}{2EJ_{1h}} \right] + \frac{e^2\lambda}{GJ_{th}}$ $K_{12} = 1.3 \left[\frac{\lambda^3}{3EJ_{1h}} + \frac{\lambda^2(d-\lambda)}{EJ_{1h}} + \frac{\lambda(d-\lambda)^2}{EJ_{1h}} + \frac{(d-\lambda)^3}{3EJ_{2h}} \right] + \frac{e^2d}{GJ_{th}}$	<p style="text-align: center;">〈Guidance Part 4〉</p> <p style="text-align: center;">CHAPTER 1 RUDDERS</p> <p style="text-align: center;">Section 4 Rudder Strength Calculation</p> <p>401. Rudder strength calculation [See Rule]</p> <p>1. ~ 6. 〈same as present〉</p> <p>7. Type E rudders(Semi spade rudder with 2-conjugate elastic support)</p> <p>(1) General data The data on the semi spade rudder with 2-conjugate elastic support models is as follows(See Fig 4.1.7 and Fig 4.1.8 of the Guidance): <u>K_{11}, K_{12}, K_{22}</u> : Rudder horn compliance constants calculated for rudder horn with 2-conjugate elastic supports The 2-conjugate elastic supports are defined in terms of horizontal displacements, y_i, by the following equations:</p> <p style="padding-left: 40px;">at the lower rudder horn bearing: <u>$y_1 = -K_{12}B_2 - K_{22}B_1$</u> at the upper rudder horn bearing: <u>$y_2 = -K_{11}B_2 - K_{12}B_1$</u></p> <p>$y_1, y_2$: Horizontal displacements at the lower and upper rudder horn bearings, respectively (m) B_1, B_2 : Horizontal support forces at the lower and upper rudder horn bearings, respectively (kN) <u>K_{11}, K_{12}, K_{22}</u> : Obtained, in m/kN, from the following formulae:</p> $K_{11} = 1.3 \frac{\lambda^3}{3EJ_{1h}} + \frac{e^2\lambda}{GJ_{th}}$ $K_{12} = 1.3 \left[\frac{\lambda^3}{3EJ_{1h}} + \frac{\lambda^2(d-\lambda)}{2EJ_{1h}} \right] + \frac{e^2\lambda}{GJ_{th}}$ $K_{22} = 1.3 \left[\frac{\lambda^3}{3EJ_{1h}} + \frac{\lambda^2(d-\lambda)}{EJ_{1h}} + \frac{\lambda(d-\lambda)^2}{EJ_{1h}} + \frac{(d-\lambda)^3}{3EJ_{2h}} \right] + \frac{e^2d}{GJ_{th}}$	<p>Correction editorial error (UR S10 Rev.7 Corr2.)</p> <p>Correction error</p> <p>Correction editorial error (UR S10 Rev.7 Corr2.)</p>

PART 6

Amendment

Note

<RULE PART 6>

CHAPTER 2 CONTROL SYSTEMS

Section 4 Computer Based Systems (2024)

407. Technical requirements on computer based systems

3. Verification of technical requirements by the Society

(1) The implementation of the technical requirements provided in **this article** is verified by the Society as part of the system description **(404. 2 (3))**, FAT **(404. 2 (7))** and SAT **(404. 3 (6))** described above.

-‘407.’ -> ‘this article’
(Eng only)

: According to the Introduction to the Classification Technical Rules, the rule mentioned as ‘407.’ is within the same article, requiring a change in the text.

Amendment

Note

〈RULE PART6〉

CHAPTER 1 ELECTRICAL EQUIPMENT

Section 1 General

103. Testing and inspection

Table 6.1.1 Electrical equipment and cables subject to the approval and test (continued) (2023)

(Notes)

(6) To be complied with note (10) in ~~the table for tests of rotating machinery of 309.16.~~ Table 6.1.10. (2018)

Section 3 Rotating Machinery

309. Testing and inspection

5. Overspeed test 【See Guidance】

Rotating machines are to withstand the overspeed test specified in ~~the following~~ Table 6.1.7 for 2 minutes.

6. Insulation resistance test

(2) The minimum values of test voltages and insulation resistances are given in ~~the following~~ Table 6.1.8. (2017)

16. Tests

The tests of rotating machinery are ~~as following table~~ given in Table 6.1.10 according to its kinds. (2024)

605. Testing and inspection

6. Insulation resistance test

Before and after the high voltage test, the insulation resistance test for all current-carrying parts are to be carried out and minimum values are to be given in ~~the following~~ Table 6.1.20.

- The numbering order for the note has been postponed, and the new table number has been added.

- The new table number has been added.

- The new table number has been added.

- The new table number has been added.

- The new table number has been added.

Amendment

Note

Section 9 Explosion-protected Electrical Equipment

901. General

4. Selection of electrical equipment according to the maximum surface temperature

(1) The electrical equipment is to be so selected that its maximum surface temperature will not reach the ignition temperature of any gas, vapour or dust which may be present. Maximum surface temperature according to temperature class of electrical equipment is ~~as following table~~ in Table 6.1.23.

- The new table number has been added.

Section 15 High Voltage Electrical Installations

1502. System Design [See Guidance]

3. Insulation

(1) Air clearance

In general, phase-to-phase air clearances and phase-to-earth air clearances between non-insulated parts of equipment are to be not less than those specified in Table ~~as below~~ 6.1.31. However, air clearance may be reduced subject to the Society's permission.

- The new table number has been added.

1504. Power Transformers

2. Test voltage of High voltage test is given in the Table 6.1.32.

- The new table number has been added.

1505. Cables [See Guidance]

2. Test voltage of High voltage test is given in the Table 6.1.33.

- The new table number has been added.

Section 16 Electric Propulsion Unit

1603. Rotating machines (2017)

1. General

(2) The rotors are to be so constructed that they will withstand for 2 minutes at an overspeed in accordance with the requirements in ~~309-5~~ Table 6.1.7. However, the overspeed of turbo-generators and electromagnetic slip-couplings is to be 120% of the rated speed.

- The reference number has been changed to the new table number .

Amendment

Note

Section 17 Tests after Installation on Board

1701. Insulation resistance test

3. Generators and motors

The insulation resistance of each generator and motor under working temperature is to be in accordance with the requirements in ~~309-6~~ Table 6.1.8.

- The reference number has been changed to the new table number

Amendment	Note
<p style="text-align: center;"><GUIDANCE PART6></p> <p style="text-align: center;">CHAPTER 1 ELECTRICAL EQUIPMENT</p> <p style="text-align: center;">Section 3 Rotating Machinery</p> <p>309. Testing and inspection</p> <p>8. In application to 309. 16 of the Rules, “the Society's permission” of notes (9) in the table Table 6.1.10 of the Guidance means type approval, test report's confirmation, etc. 【See Rule】</p> <p>9. In application to 309. 16 of the Rules, “the Society's permission” of notes (10) in the table Table 6.1.10 of the Guidance means type approval, design approval's confirmation, etc. 【See Rule】</p> <p style="text-align: center;">Section 9 Explosion-protected Electrical Equipment</p> <p>902. Special requirements 【See Rule】</p> <p>The wording “as deemed appropriate by the Society” in 902. of the Rules means the followings.</p> <p>1. Flameproof type electrical equipment</p> <p>(5) When installing equipment, its flameproof joints are not to be installed within the distance specified in the following table Table 6.1.8 of the Guidance with respect to a bulkhead or solid object.</p> <p style="text-align: center;">Section 15 High Voltage Electrical Installations</p> <p>1501. General 【See Rule】</p> <p>1. The supply voltages and frequency specified in the followings Table 6.1.19 of the Guidance are recognized as a standard.</p>	<p>- The numbering order for the note has been postponed , and the reference has been changed to the new table number.</p> <p>- The reference has been changed to the new table number.</p> <p>- The reference has been changed to the new table number.</p>

PART 7

Present	Amendment	Note
<p style="text-align: center;">Present</p> <p style="text-align: center;"><Guidance> Pt 7</p> <p style="text-align: center;">ANNEX 7-2 Guidance for the Container Securing Arrangements</p> <p>8. Determination and application of forces</p> <p>(1) Symbols and definitions (2019)</p> <p>(A) Definitions and symbols of terms are as follows.</p> <p style="text-align: center;">T_{θ}, T_{ϕ} : full period of <u>pitch and roll</u> of the ship (sec)</p> <p style="text-align: center;">Annex 7-12 Liquefaction Ore Bulk Cargoes</p> <p>3. Hull Strength</p> <p>(5) Corrugated bulkheads</p> <p>(A)</p> <p>Face part: $C = \frac{1.5}{\sqrt{1 + \left(\frac{t_w}{t_f}\right)^2}}$</p> <p>Web part: $C = 1.0$</p> <p>t_f, t_w = thickness of plates of face part and web part, respectively (mm).</p>	<p style="text-align: center;">Amendment</p> <p style="text-align: center;"><Guidance> Pt 7</p> <p style="text-align: center;">ANNEX 7-2 Guidance for the Container Securing Arrangements</p> <p>8. Determination and application of forces</p> <p>(1) Symbols and definitions (2019)</p> <p>(A) Definitions and symbols of terms are as follows.</p> <p style="text-align: center;">T_{θ}, T_{ϕ} : full period of <u>roll and pitch</u> of the ship (sec)</p> <p style="text-align: center;">Annex 7-12 Liquefaction <u>of</u> Ore Bulk Cargoes</p> <p>3. Hull Strength</p> <p>(5) Corrugated bulkheads</p> <p>(A)</p> <p>Face part: $C = \frac{1.4}{\sqrt{1 + \left(\frac{t_w}{t_f}\right)^2}}$</p> <p>Web part: $C = 1.0$</p> <p>t_f, t_w = thickness of plates of face part and web part, respectively (mm).</p>	<p style="text-align: center;">Note</p> <p style="text-align: center;">- English only</p>

PART 7 (CH5, 6)

현 행

〈Rules〉 Pt 7 Ch 5

CHAPTER 5 LIQUEFIED GASS CARRIERS

103. Equivalentents

The construction and equipment, etc. which do not fall under the provisions of this Chapter but are considered to be equivalent to those required in this Chapter will be accepted by the Society.

305. Access to spaces in the cargo area (IGC Code 3.5)

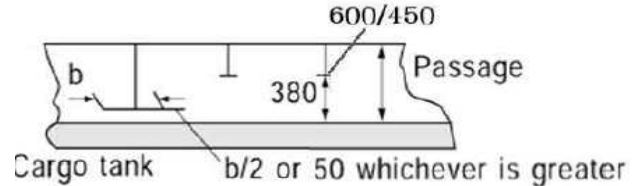


Fig 7.5.8

개 정 안

〈Rules〉 Pt 7 Ch 5

CHAPTER 5 LIQUEFIED GASS CARRIERS

103. Equivalentents

The equivalence of alternative and novel features which deviate from or are not directly applicable to the Rules is to be in accordance with Pt 1, Ch 1 105. of Rules for the Classification of Steel Ships.

305. Access to spaces in the cargo area (IGC Code 3.5)

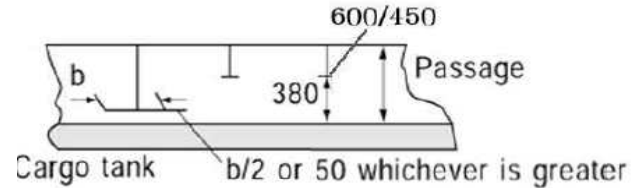


Fig 7.5.8

비 고

Present	Amendment	Note
<p data-bbox="360 215 712 248" style="text-align: center;"><Guidance> Pt 7 Ch 5</p> <p data-bbox="136 309 936 347" style="text-align: center;">CHAPTER 5 LIQUEFIED GASS CARRIERS</p> <p data-bbox="96 411 421 437">420. Construction process</p> <p data-bbox="125 464 920 489">6. Additional information on the gas-trial and cargo full loading test</p> <p data-bbox="159 536 976 624">(4) The cargo full loading test to capacity specified in the preceding (1) (B) may be conducted simultaneously with the gas-trial indicated in the preceding (1) (A).</p> <p data-bbox="159 632 976 807">(5) The survey items "at loading operation" specified in Table 7.5.6 of the Guidance in the preceding (1) (B) may be substituted by the test items which were carried out during on board test and gas trial, and the survey items on "Condition of cargo tanks and other cargo containment systems after full loading" may be confirmed when the inspection for "discharging operation" is carried out.</p>	<p data-bbox="1272 215 1624 248" style="text-align: center;"><Guidance> Pt 7 Ch 5</p> <p data-bbox="1048 277 1848 316" style="text-align: center;">CHAPTER 5 LIQUEFIED GASS CARRIERS</p> <p data-bbox="1003 379 1328 405">420. Construction process</p> <p data-bbox="1032 432 1832 458">6. Additional information on the gas-trial and cargo full loading test</p> <p data-bbox="1070 504 1888 592">(4) The cargo full loading test to capacity specified in the preceding (1) (B) may be conducted simultaneously with the gas-trial indicated in the preceding (1) (A).</p> <p data-bbox="1070 600 1888 775">(5) The survey items at loading operation in the preceding (1) (B) may be substituted by the test items which were carried out during on board test and gas trial, and the survey items on "Condition of cargo tanks and other cargo containment systems after full loading" may be confirmed when the inspection for "discharging operation" is carried out.</p>	

Present	Amendment	Note
<p style="text-align: center;">(Guidance) Pt 7 Ch 5</p> <p style="text-align: center;">Annex 7A-8 Guidelines for Safety Margin of Cargo Containment System</p> <p style="text-align: center;">CHAPTER 2 SAFETY MARGIN</p> <p style="text-align: center;">Section 1 Type A Independent Tanks</p> <p>201. Allowable stress for ultimate and accidental design conditions</p> <p>The allowable membrane equivalent stresses for primarily constructed of plane surfaces, applied for finite element analysis, shall not exceed a lesser of $0.83R_e$ or $0.5R_m$ for nickel steels and carbon-manganese steels and a lesser of $0.83R_e$ or $0.4R_m$ for austenitic steels and aluminium alloys. The thickness of the skin plate and the size of the stiffener shall not be less than those required for type A independent tanks. <u>If 9% nickel steel is used for the plates of the cargo tank, the allowable stress $0.75R_e$ is applied to the calculation of the tank plates.</u></p> <p style="text-align: center;">Section 3 Type C Independent Tanks</p> <p>301. Allowable stress for ultimate and accidental design conditions</p> <p><u>For horizontal cylindrical tanks made of C-Mn steel supported in saddles, the equivalent stress, σ_e, in the stiffening rings shall not exceed a lesser of $0.85R_e$ or $0.57R_m$ if calculated using finite element method:</u></p> $\sigma_e = \sqrt{(\sigma_n + \sigma_b)^2 + 3\tau^2}$ <p>where,</p> <p>σ_n : nominal stress in the circumferential direction of the stiffening ring(N/mm²)</p> <p>σ_b : bending stress in the circumferential direction of the stiffening ring(N/mm²)</p> <p>τ : shear stress in the stiffening ring(N/mm²)</p>	<p style="text-align: center;">(Guidance) Pt 7 Ch 5</p> <p style="text-align: center;">Annex 7A-8 Guidelines for Safety Margin of Cargo Containment System</p> <p style="text-align: center;">CHAPTER 2 SAFETY MARGIN</p> <p style="text-align: center;">Section 1 Type A Independent Tanks</p> <p>201. Allowable stress for ultimate and accidental design conditions</p> <p>The allowable membrane equivalent stresses for primarily constructed of plane surfaces, applied for finite element analysis, shall not exceed a lesser of $0.83R_e$ or $0.5R_m$ for nickel steels and carbon-manganese steels and a lesser of $0.83R_e$ or $0.4R_m$ for austenitic steels and aluminium alloys. The thickness of the skin plate and the size of the stiffener shall not be less than those required for type A independent tanks.</p> <p style="text-align: center;">Section 3 Type C Independent Tanks</p> <p>301. Allowable stress for ultimate and accidental design conditions</p> <p style="text-align: center;">(delete)</p>	

Present	Amendment	Note
<p style="text-align: center;">Present</p> <p style="text-align: center;"><Guidance> Pt 7 Ch 5</p> <p style="text-align: center;">Section 4 Membrane Type Tanks</p> <p>402. Allowable stress and buckling pressure of membrane systems</p> <p>Sloshing load due to ship motion is governing factor in comparison with other loads such as cooling-down, ship loading, vibration, static heel or collision case. In order to evaluate the structural strength of membrane, PUF, plywood and mastic in cargo containment system against sloshing load for ultimate and accidental design conditions, the following criteria is recommended.</p> <ul style="list-style-type: none"> - allowable equivalent stress : $\sigma_{eq} \leq 0.67R_e$ - allowable buckling pressure : $P_c < 0.9P_{cr}$ <p>P_{cr} is the critical buckling pressure which should be based on the acknowledged experimental data for each material and the standard recognized by the Society</p>	<p style="text-align: center;">Amendment</p> <p style="text-align: center;"><Guidance> Pt 7 Ch 5</p> <p style="text-align: center;">Section 4 Membrane Type Tanks</p> <p>402. Allowable stress and buckling pressure of membrane systems</p> <p>Sloshing load due to ship motion is governing factor in comparison with other loads such as cooling-down, ship loading, vibration, static heel or collision case. In order to evaluate the structural strength of membrane, PUF, plywood and mastic in cargo containment system against sloshing load for ultimate and accidental design conditions, the following criteria is recommended.</p> <ul style="list-style-type: none"> - allowable equivalent stress : $\sigma_{eq} \leq 0.60R_e$ - allowable buckling pressure : $P_c < 0.9P_{cr}$ <p>P_{cr} is the critical buckling pressure which should be based on the acknowledged experimental data for each material and the standard recognized by the Society</p>	

PART 8

Present	Amendment	Note
<p style="text-align: center;"><Guidance Pt 8></p> <p style="text-align: center;">CHAPTER 7 CONTAINMENT OF FIRE</p> <p style="text-align: center;">Section 1 ~ Section 5 <omitted> Section 6 Ventilation Systems [See Rule]</p> <p>601. General <omitted></p> <p>602. Arrangement of ducts</p> <ol style="list-style-type: none"> 1. In applying 602. 4 of the Rules, "A-60" class insulation" is, as a standard, to be an insulation with rock-wool approved as non-combustible material, or insulation approved as "A-60" class standard and arrangement of ducts are to be in accordance with Fig 8.7.5 of the Guidance. 2. In applying 602. and 605. of the Rules for determining fire insulation for trunks and ducts which pass through an enclosed space, the term "pass through" means the part of the trunk/duct contiguous to the enclosed space. (see Fig 8.7.6 of the Guidance.) 	<p style="text-align: center;"><Guidance Pt 8></p> <p style="text-align: center;">CHAPTER 7 CONTAINMENT OF FIRE</p> <p style="text-align: center;">Section 1 ~ Section 5 <same as the present> Section 6 Ventilation Systems [See Rule]</p> <p>601. General <same as the present></p> <p>602. Arrangement of ducts</p> <ol style="list-style-type: none"> 1. In applying 602. 4 of the Rules, "A-60" class insulation" is, as a standard, to be an insulation with rock-wool approved as non-combustible material, or insulation approved as "A-60" class standard and arrangement of ducts are to be in accordance with Fig 8.7.5 of the Guidance. 2. In applying 602. and 605. 1 & 2 of the Rules for determining fire insulation for trunks and ducts which pass through an enclosed space, the term "pass through" means the part of the trunk/duct contiguous to the enclosed space. (see Fig 8.7.6 of the Guidance.) 	

PART 13

Present	Amendment	Note
<p style="text-align: center;"><RULE PART 13></p> <p style="text-align: center;">Sub-Part 1</p> <p style="text-align: center;">Chapter 5 HULL GIRDER STRENGTH</p> <p style="text-align: center;">Section 1 HULL GIRDER YIELDING STRENGTH</p> <p>SYMBOLS</p> <p>For symbols not defined in this section, refer to Ch 1, Sec 4. <omitted></p> <p>$\underline{f_B}$: Heading correction factor, to be taken as: $\underline{f_B} = 1.05$ for seagoing conditions. $\underline{f_B} = 1.0$ for ballast water exchange at sea, harbour/sheltered water and accidental flooded design load scenarios.</p>	<p style="text-align: center;"><RULE PART 13></p> <p style="text-align: center;">Sub-Part 1</p> <p style="text-align: center;">Chapter 5 HULL GIRDER STRENGTH</p> <p style="text-align: center;">Section 1 HULL GIRDER YIELDING STRENGTH</p> <p>SYMBOLS</p> <p>For symbols not defined in this section, refer to Ch 1, Sec 4. <same as the present></p> <p>$\underline{f_{\beta}}$: Heading correction factor, to be taken as: $\underline{f_{\beta}} = 1.05$ for seagoing conditions. $\underline{f_{\beta}} = 1.0$ for ballast water exchange at sea, harbour/sheltered water and accidental flooded design load scenarios.</p>	<p>- Heading correction factor, f_B replaced with f_{β} (English only)</p>

OTHER RULES AND GUIDANCE

Present	Amendment	Note
<p data-bbox="241 252 987 295">〈Guidance for Floating Production Units〉</p> <p data-bbox="389 325 837 363">CHAPTER 1 GENERAL</p> <p data-bbox="477 429 748 462">Section 1 General</p> <p data-bbox="226 501 557 528">102. Classification of units</p> <p data-bbox="248 542 479 569">1. Purpose of units</p> <p data-bbox="271 592 754 619">(3) FSO (Floating Production and Storage)</p> <p data-bbox="324 633 999 699">FSO is a unit with systems for the storage and offloading of produced crude oil and petroleum gases.</p>	<p data-bbox="1059 252 1805 295">〈Guidance for Floating Production Units〉</p> <p data-bbox="1207 325 1655 363">CHAPTER 1 GENERAL</p> <p data-bbox="1294 429 1565 462">Section 1 General</p> <p data-bbox="1028 501 1359 528">102. Classification of units</p> <p data-bbox="1050 542 1281 569">1. Purpose of units</p> <p data-bbox="1072 592 1556 619">(3) FSO (Floating Storage and Offloading)</p> <p data-bbox="1126 633 1834 699">FSO is a unit with systems for the storage and offloading of produced crude oil and petroleum gases.</p>	<p data-bbox="1861 557 2107 620">– Edited for translation error.</p>

Present	Amendment	Note
<p data-bbox="315 220 757 252" style="text-align: center;">〈Guidance for Type Approval〉</p> <p data-bbox="248 312 824 352" style="text-align: center;">CHAPTER 3 TYPE APPROVAL</p> <p data-bbox="96 408 976 467">2504. Test requirements of additional special feature notation HHS(High Holding Securing) (2021)</p> <p data-bbox="125 488 976 639">6. The twistlock housing should be fastened with at least one bolt each at the top and bottom. Also the dimension of the neck of the twist lock should be equal to or greater than the value according to Fig. 3.25.5. In this case, the neck of the twistlock should be symmetrical in the length/width direction. (2023)</p> <div data-bbox="349 703 745 1042" style="text-align: center;"> </div> <p data-bbox="443 1074 658 1106" style="text-align: center;">Fig. 3.25.5 (2024)</p> <p data-bbox="219 1214 853 1254" style="text-align: center;">CHAPTER 4 DESIGN APPROVAL</p> <p data-bbox="174 1310 898 1342" style="text-align: center;">Section 3 Container Lashing <u>calculation program</u></p>	<p data-bbox="1223 220 1664 252" style="text-align: center;">〈Guidance for Type Approval〉</p> <p data-bbox="1155 312 1731 352" style="text-align: center;">CHAPTER 3 TYPE APPROVAL</p> <p data-bbox="1003 408 1883 467">2504. Test requirements of additional special feature notation HHS(High Holding Securing) (2021)</p> <p data-bbox="1032 488 1883 639">6. The <u>bottom</u> twistlock housing should be fastened with at least one bolt each at the top and bottom. Also the dimension of the neck of the twist lock should be equal to or greater than the value according to Fig. 3.25.5. In this case, the neck of the twistlock should be symmetrical in the length/width direction. (2023)</p> <div data-bbox="1223 667 1675 951" style="text-align: center;"> </div> <p data-bbox="1328 983 1565 1015" style="text-align: center;">그림 3.25.5 (2024)</p> <p data-bbox="1126 1206 1760 1246" style="text-align: center;">CHAPTER 4 DESIGN APPROVAL</p> <p data-bbox="1081 1302 1805 1334" style="text-align: center;">Section 3 Container Lashing Calculation Program</p>	<p data-bbox="1917 1246 2074 1270" style="text-align: center;">– English only</p>